



Chapter 2 Kinematics of particles and rigid bodies

(2-5) 2.4 Kinematics of planar mechanisms

Bachelor Program in AUTOMATION ENGINEERING

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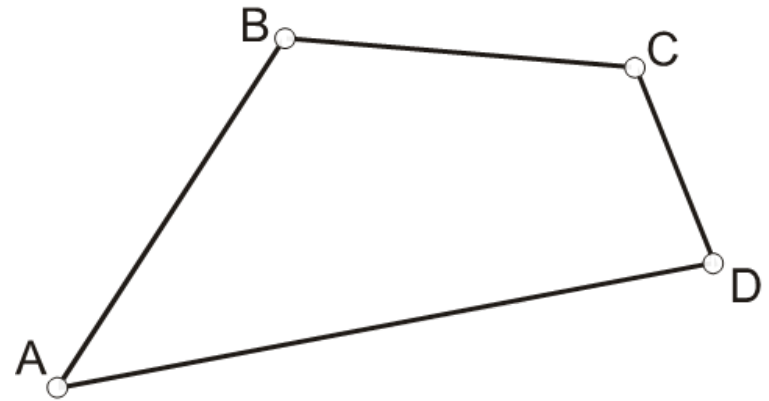
First Semester, 2014-2015



2.4 Kinematics of planar mechanisms (performed with dynamic analysis in Chapter 4)

- A free four-bar linkage
- This system has 12 d.o.f. and 8 degrees of constraints, i.e. three d.o.f. as a whole rigid body and one internal d.o.f. (“deformability” of the system).

- ⌋ Four-bar linkage without any fixed body, with complete freedoms;
- ⌋ Every rigid body:
 - 1) translation motion freedom along x axis + translation motion freedom along y axis + revolution freedom around z axis = 3 dof/body;
Further, $3 \text{ dof/body} * 4 \text{ body} = 12 \text{ dof /system}$;
 - 2) 8 constraints = (revolution constraint around x axis + revolution constraint around y axis) * 4;
- ⌋ Internal dof belongs to the system, is to generate motion then deform the system; is only another expression;



Free four-bar linkage,
without frame



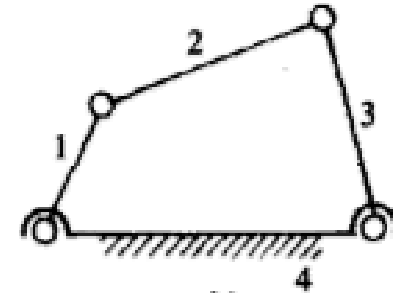
To fix a body, the free four-bar linkage is left with 1 residual dof.

2D)

$$l = 3(m - 1) - 2c_1 - c_2$$

m = number of links

c_i = number of joints
leaving i DOFs free



$l = 1$

Four-bar linkage

$$l = 3(m - 1) - 2c_1 - c_2$$

$$m = 4$$

$$c_1 = 1 + 1 + 1 + 1 = 4$$

$$c_2 = 0$$

therefore

$$l = 3(4 - 1) - 2 \cdot 4 - 0 = 1$$

Clockwise analysis : To calculate c_1

- Joint 1-2: between link 1 and 2, only revolution around shaft, leaving 1 DOF free, then count as 1;
- Joint 2-3: between link 2 and 3, only revolution, leaving 1 DOF free, then count as 1;
- Joint 3-4: between link 3 and 4, only revolution, leaving 1 DOF free, then count as 1;
- Joint 4-1: between link 4 and 1, only revolution, leaving 1 DOF free, then count as 1;



Collection of planar mechanisms

- A collection of rigid bodies properly constrained can be used to create a mechanism.

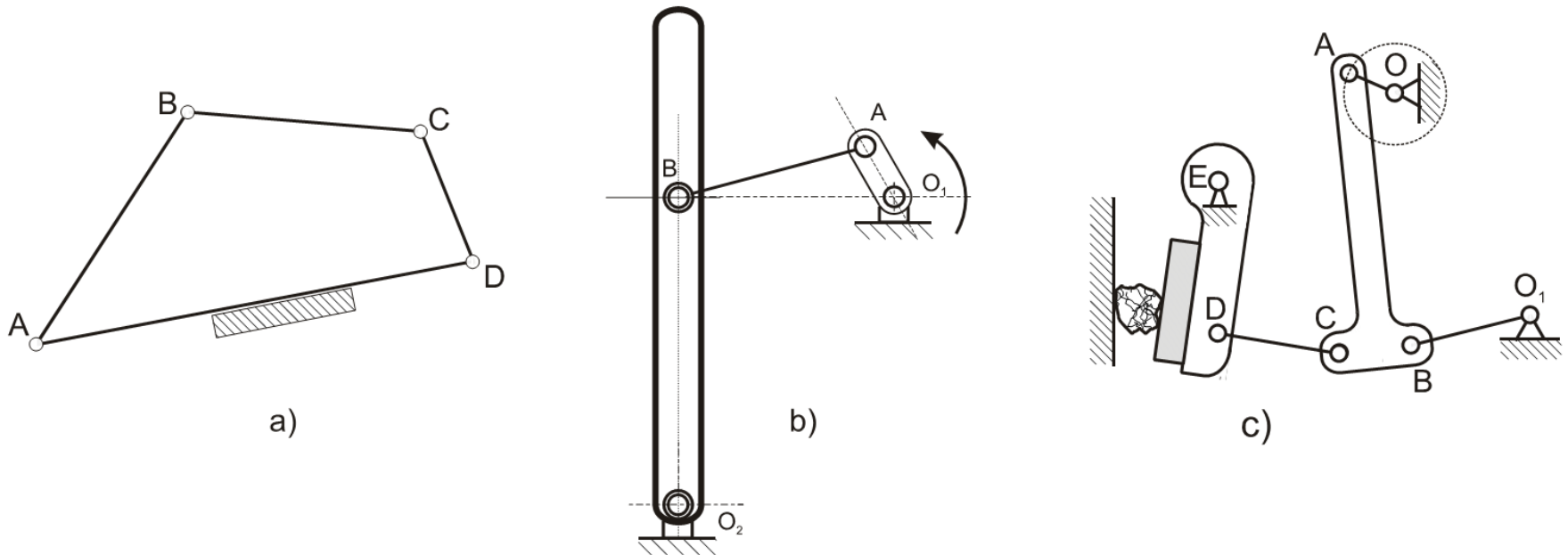
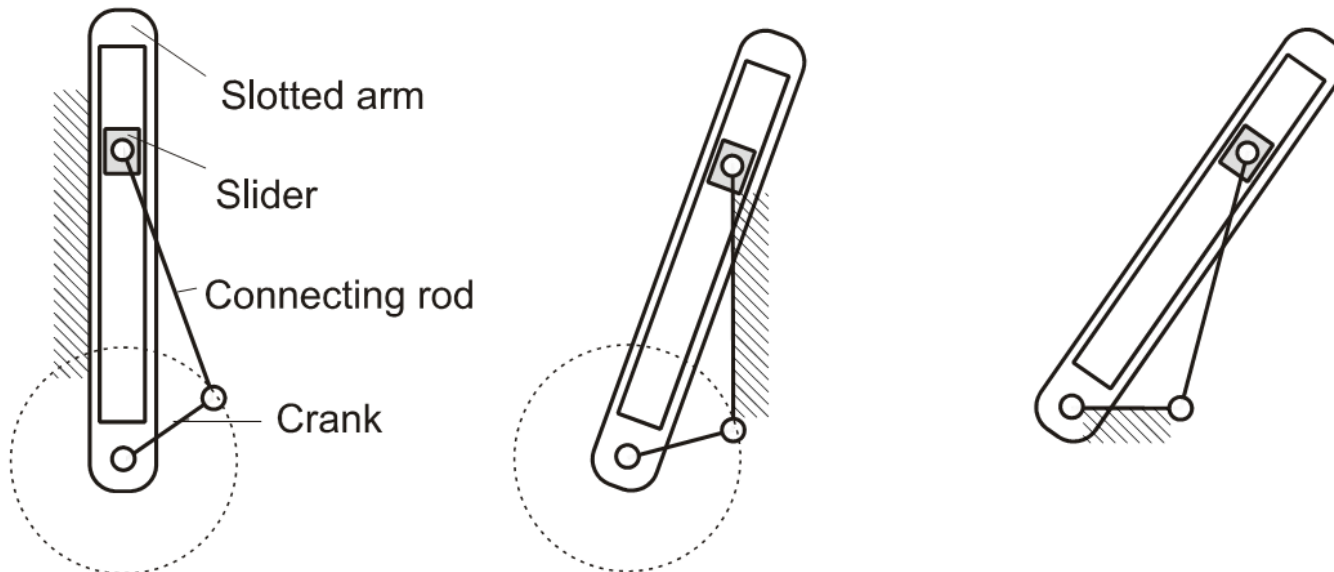


Fig. 2.24



Slider-slotted arm mechanism

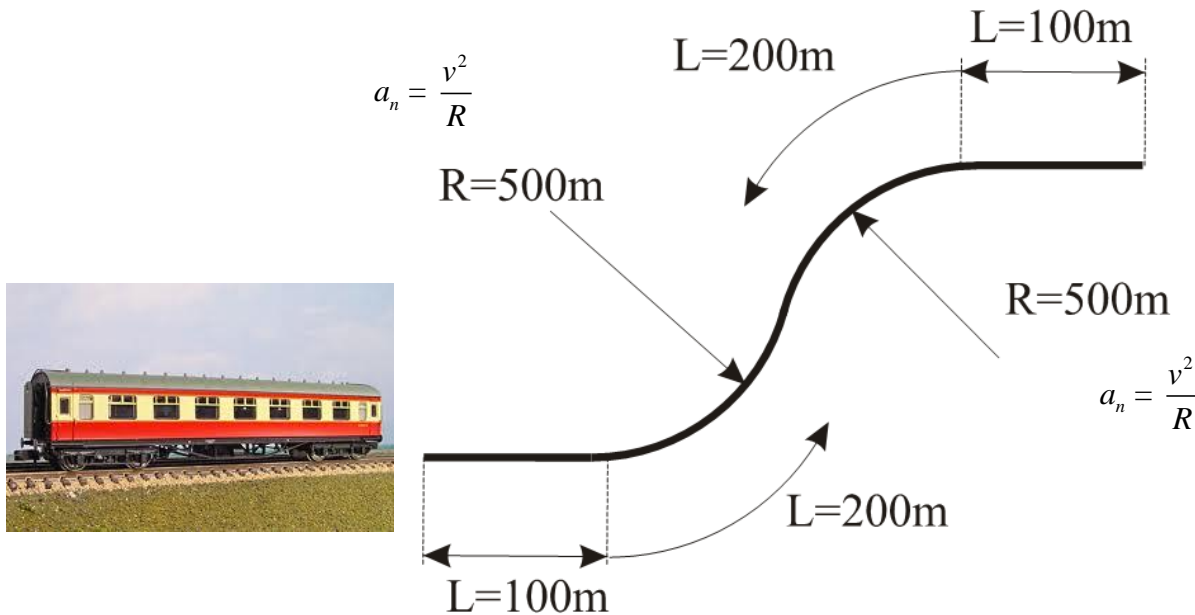
- Four rigid bodies: a slotted arm, a slotted arm, a crank, a connecting rod and a slider ;
- Overall 12 dof: same with four-bar linkage;
- 4 double constraints: 8 constraints = (revolution constraint around x axis + revolution constraint around y axis) * 4; caused by 3 pins and 1 joke (slider);
- To constrain 1 body, then 1 dof left, some diffused mechanisms





2.5 Kinematics of a particle and of rigid bodies: applications

- 1) Motion of a particle on a curvilinear path
- A railway coach moves along the track indicated in the figure below at a constant speed of 20 m/s.
- By considering the coach as a particle, **determine the acceleration** to which the passengers are submitted in the various parts of the track.





Principle : circular motion

- Particle P moves along a circular trajectory, with center O, radius R;
- Assume complex coordinate system coincident with center O;
- Simple to particle P position in polar coordinates;

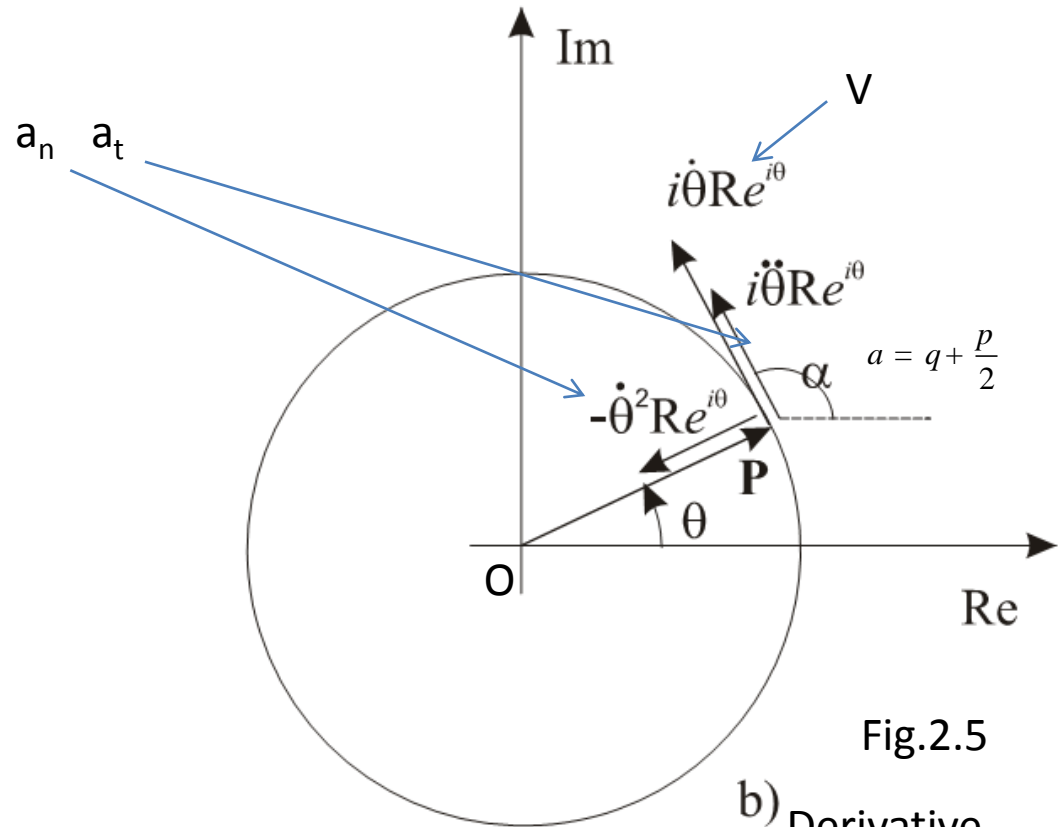


Fig.2.5

$$\begin{aligned} \bar{P} &= R \cos \theta + i R \sin \theta = R e^{i\theta} \\ \bar{V} &= i \dot{\theta} R e^{i\theta} \\ \bar{a} &= i \ddot{\theta} R e^{i\theta} - \dot{\theta}^2 R e^{i\theta} \end{aligned}$$

b) Derivative direction,
0 order,
1 order,
2 order of position



Calculation

- Some correction: add a line between s_2 and s_4 , and assume tangent with s_2 and s_4 ;
- Determine the acceleration in parts: s_1 to s_5

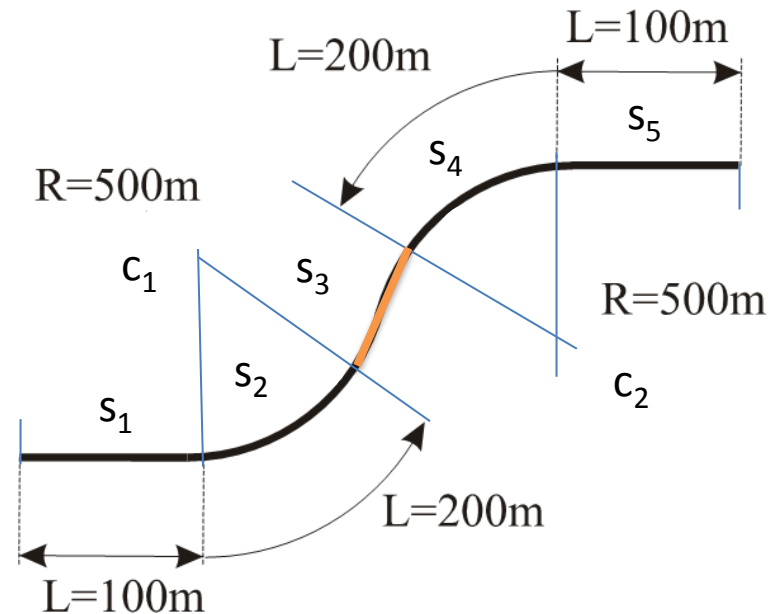
In s_1 , acceleration $a_{s_1} = 0$, as velocity $v_{s_1} = 20\text{m/s}$ and non direction change;

In s_2 , acceleration $a_{s_2} = -\dot{q}^2 Re^{iq} = -\frac{v^2}{R} e^{iq}$, the mangitude $\frac{v^2}{R} = \frac{20^2}{500} = 0.8\text{m/s}^2$,
 acceleration direction is to c_1 , as velocity $v_{s_2} = 20\text{m/s}$ and direction changes along circle c_1 ;

In s_3 , acceleration $a_{s_3} = 0$, as velocity $v_{s_3} = 20\text{m/s}$ and non direction change;

In s_4 , acceleration $a_{s_4} = -\dot{q}^2 Re^{iq} = -\frac{v^2}{R} e^{iq}$, the mangitude $\frac{v^2}{R} = \frac{20^2}{500} = 0.8\text{m/s}^2$,
 acceleration direction is to c_2 , as velocity $v_{s_4} = 20\text{m/s}$ and direction changes along circle c_2 ;

In s_5 , acceleration $a_{s_5} = 0$, as velocity $v_{s_5} = 20\text{m/s}$ and non direction change;





2) Law of motion

- The load of a **lifting plant** has to be lifted of 24 m starting from idle condition and ending its run at null velocity, with a trapezoidal law of motion.
- The maximum lifting speed is 10 m/min, while the transient motions at the beginning and at the end of the run last 2 s **respectively**.
- **The diagrams of velocity and acceleration are requested, together with the necessary run time.**





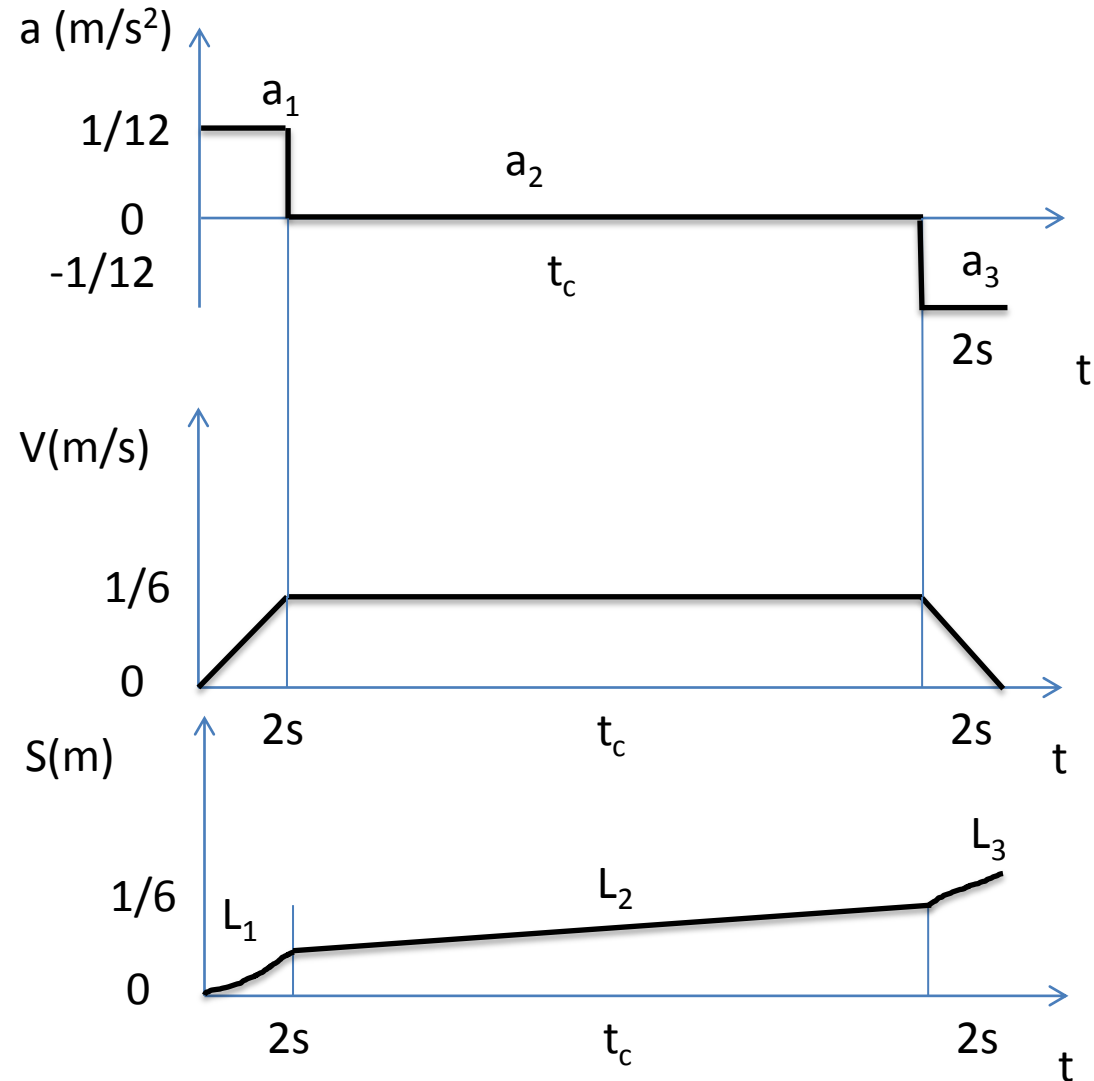
Calculation

- $V_c = 10 \text{ m/min} = 1/6 \text{ m/s}$

$$a_1 = V_c / 2s = 1/6 / 2 = 1/12 \text{ m/s}^2$$

$$a_2 = 0;$$

$$a_3 = -V_c / 2s = -1/6 / 2 = -1/12 \text{ m/s}^2$$



$$L = L_1 + L_2 + L_3 = \int_0^{2s} a_1 t dt + V_c t_c + \int_0^{2s} |a_3| t dt$$

$$24 = a_1 \frac{1}{2} t^2 \Big|_0^{2s} + V_c t_c + |a_3| \frac{1}{2} t^2 \Big|_0^{2s} = \frac{1}{12} \frac{1}{2} t^2 \Big|_0^{2s} + \frac{1}{6} t_c + |-\frac{1}{12}| \frac{1}{2} t^2 \Big|_0^{2s}$$

$$24 = \frac{1}{3} + \frac{1}{6} t_c$$

$$t_c = (24 - \frac{1}{3}) * 6 = 142s$$

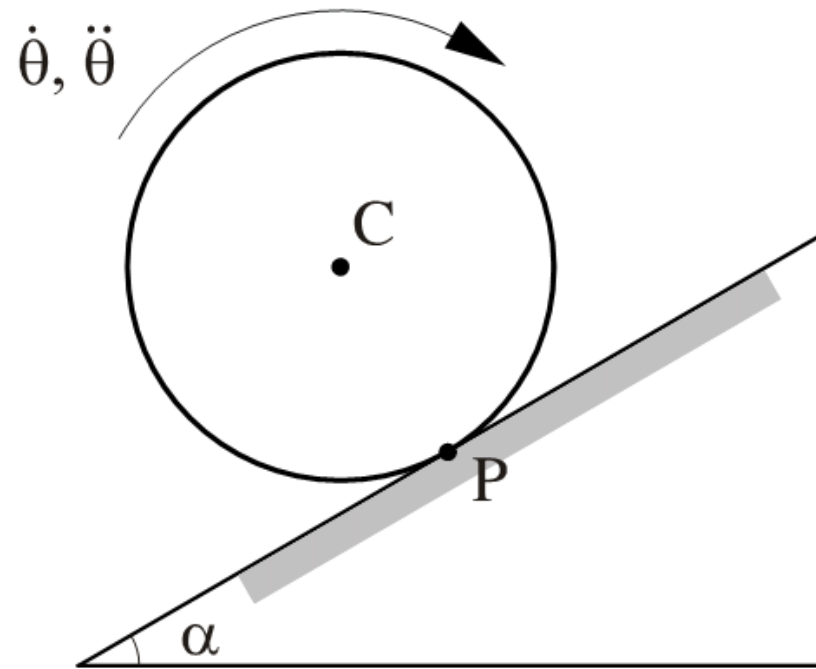


3) Rolling without slipping

- A disc of radius R rolls without slipping on an inclined plane (see figure below).

Given its angular velocity $\dot{\theta}$ and its angular acceleration $\ddot{\theta}$ to determine.

1. the trajectory of the center C of the disc;
2. the instantaneous center of velocity of the disc;
3. velocity and acceleration of the center C of the disc;
4. the acceleration of point P of the disc contacting the plane





Calculation

1. the trajectory of the center C of the disc;

$$p_c(t) = p_p(t) + (P - C) = r e^{ia} + R e^{i(a + \frac{p}{2})} = \int_0^t R \dot{q} t e^{ia} dt + R e^{i(a + \frac{p}{2})}$$

2. the instantaneous center of velocity of the disc;

point P, as P is the point of the disc has a null velocity in considered instant time;

3. velocity and acceleration of the center C of the disc;

$$V_c(t) = v e^{ia} = R \dot{q} t e^{ia};$$

$$a_c(t) = a e^{ia} = R \ddot{q} t e^{ia};$$

4. the acceleration of point P of the disc contacting the plane

$V_p(t) = 0$, as point P contacts with inclined plane

$$a_p(t) = a_c + \ddot{q} (P - C) - (\dot{q})^2 (P - C) = R \ddot{q} t e^{ia} + \ddot{q} R e^{i(a + \frac{p}{2})} - (\dot{q})^2 R e^{i(a + \frac{p}{2})};$$

